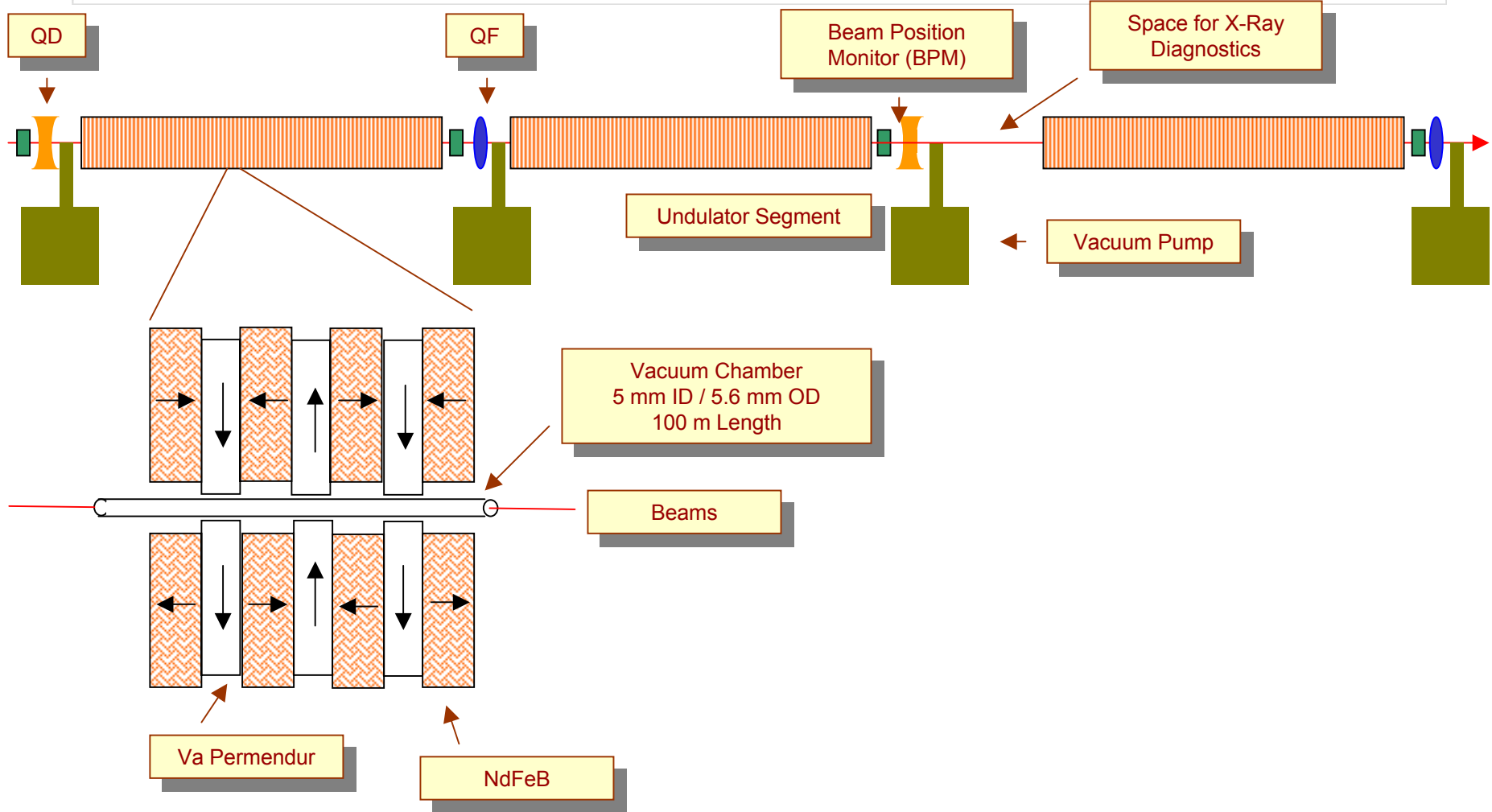


Undulator Chamber Wakefields

Heinz-Dieter Nuhn, SLAC / SSRL
December 10, 2001

- Undulator Chamber Wakefield Description
- Effects on FEL Performance
- Consequences for the LCLS

LCLS Undulator



Undulator Chamber Wakefield Sources

- ***Geometric Wakefields***
- ***Surface Roughness Wakefields***
- ***Resistive Wall Wakefields***

Geometric Undulator Chamber Wakefields

Calculations for Short Bunches Based on Diffraction Wakefield Model

$$\langle W_z^{diff} \rangle \approx \frac{\Gamma(1/4)}{4\pi^{5/2}} \frac{Z_0 c M}{a L} \sqrt{\frac{g}{\sigma_z}}, \quad \sigma_z / a \ll 1 \quad (W_z^{diff})_{rms} \approx (0.40) \langle W_z^{diff} \rangle$$

$$\langle W_x^{diff} \rangle \approx (0.463) \frac{Z_0 c M}{\pi^3 a^3 L} \sqrt{g \sigma_z}, \quad \sigma_z / a \ll 1$$

W_z	Average Wakefield Green's Function [V/C/m]
L	Total Undulator Length
Z_0	Vacuum Impedance
a	Pipe Radius
σ	Conductivity of Vacuum Chamber Material ($5.9 \times 10^7 \Omega^{-1}\text{m}^{-1}$ for Copper)
M	Number of Gaps / BPMs / Pump Slots

Geometric Undulator Chamber Wakefields

Flange Gaps

Gap Length : $g = 0.25 \text{ mm}$

Number of Flange Gaps : $M = 144$

$$\langle \delta \rangle = \frac{e^2 NL \langle W_z^{diff} \rangle}{E} = 0.008\%$$

$$\sigma_\delta = \frac{e^2 NL (W_z^{diff})_{rms}}{E} = 0.003\%$$

$$\Delta \varepsilon_n = 0.008\% \quad \text{for } 100 \mu\text{m oscillation}$$

RF Cavity BPMs

Gap Length : $g = 5 \text{ mm}$

Number of Flange Gaps : $M = 72$

$$\langle \delta \rangle = \frac{e^2 NL \langle W_z^{diff} \rangle}{E} = 0.019\%$$

$$\sigma_\delta = \frac{e^2 NL (W_z^{diff})_{rms}}{E} = 0.007\%$$

$$\Delta \varepsilon_n = 0.007\% \quad \text{for } 100 \mu\text{m oscillation}$$

Pump Slots

Gap Length : $g = 5 \text{ mm}$

Number Pumping Slots per segment: ~ 10

Total Number of Pumping Slots: $M = 360$

Slot width $w = 1 \text{ mm}$

Azimuthal Filling Factor: $w/2\pi a = 0.064$

$$\langle \delta \rangle = \frac{w}{2\pi a} \frac{e^2 NL \langle W_z^{diff} \rangle}{E} = 0.006\%$$

$$\sigma_\delta = \frac{w}{2\pi a} \frac{e^2 NL (W_z^{diff})_{rms}}{E} = 0.002\%$$

$$\Delta \varepsilon_n = 0.006\% \quad \text{for } 100 \mu\text{m oscillation}$$

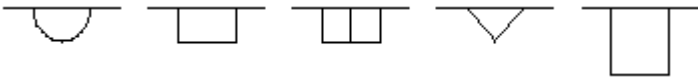
Shielded Bellows (Total Number: ~ 36)

Negligible due to Shielding

Amplitudes negligibly small.

Vacuum Chamber Surface Roughness

Initial Bump Model for Surface Roughness => Aspect Ratio ~ 1/1

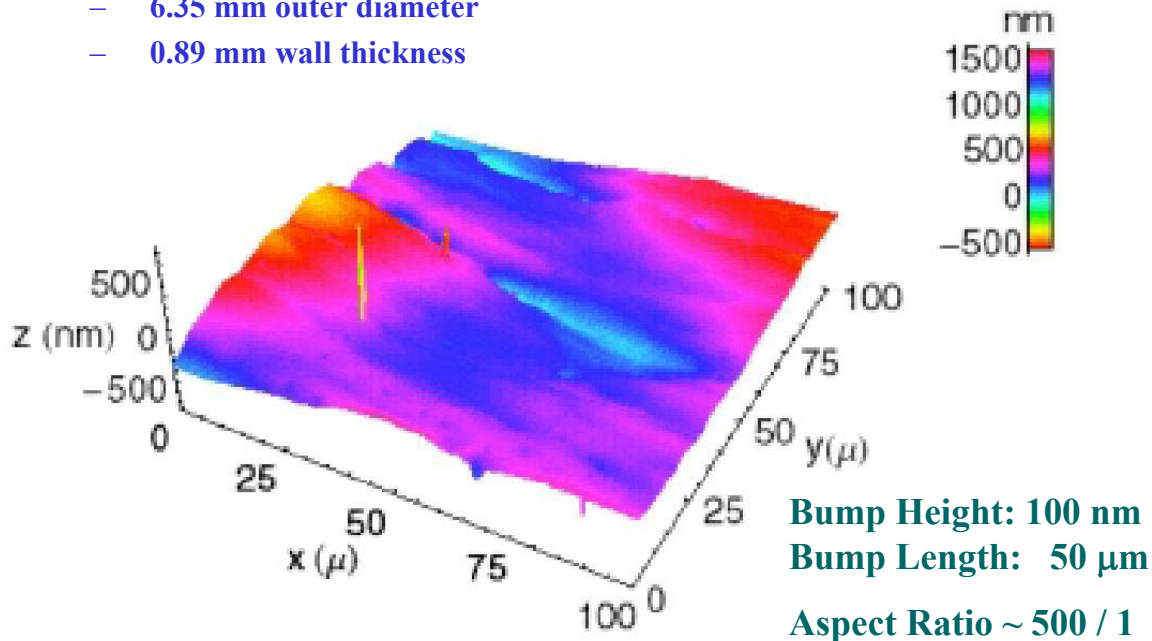


=> Large Wakefield Amplitudes

AFM Measurement of Surface Roughness

Type 316-L Stainless Steel Tubing VALEX Corp. (best commercial finish, A5)

- 6.35 mm outer diameter
- 0.89 mm wall thickness



=> Small Wakefield Amplitudes

Atomic Force Microscope (AFM) Measurements show much smaller Aspect Ratios Surface Roughness Wake becomes unimportant

Wall Roughness Wakefields

Sinusoidal Corrugation – Arbitrary Bunch Length Model (G. Stupakov, 2000)

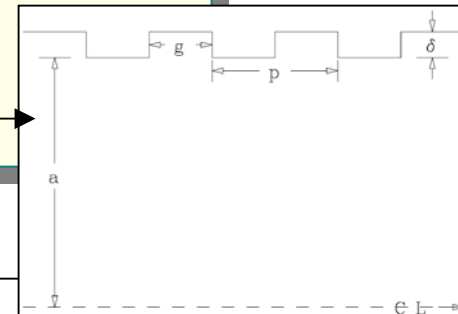
$$W_z(s) = cZ_0 e^2 \frac{h_0^2 \kappa^{3/2}}{a} \frac{1}{2\sqrt{\pi}} \frac{\partial}{\partial s} \frac{1}{\sqrt{s}} \left[\cos\left(\frac{\kappa s}{2}\right) + \sin\left(\frac{\kappa s}{2}\right) \right]$$

Synchronous Mode (A. Novokhatski, A. Mosnier, 1996)

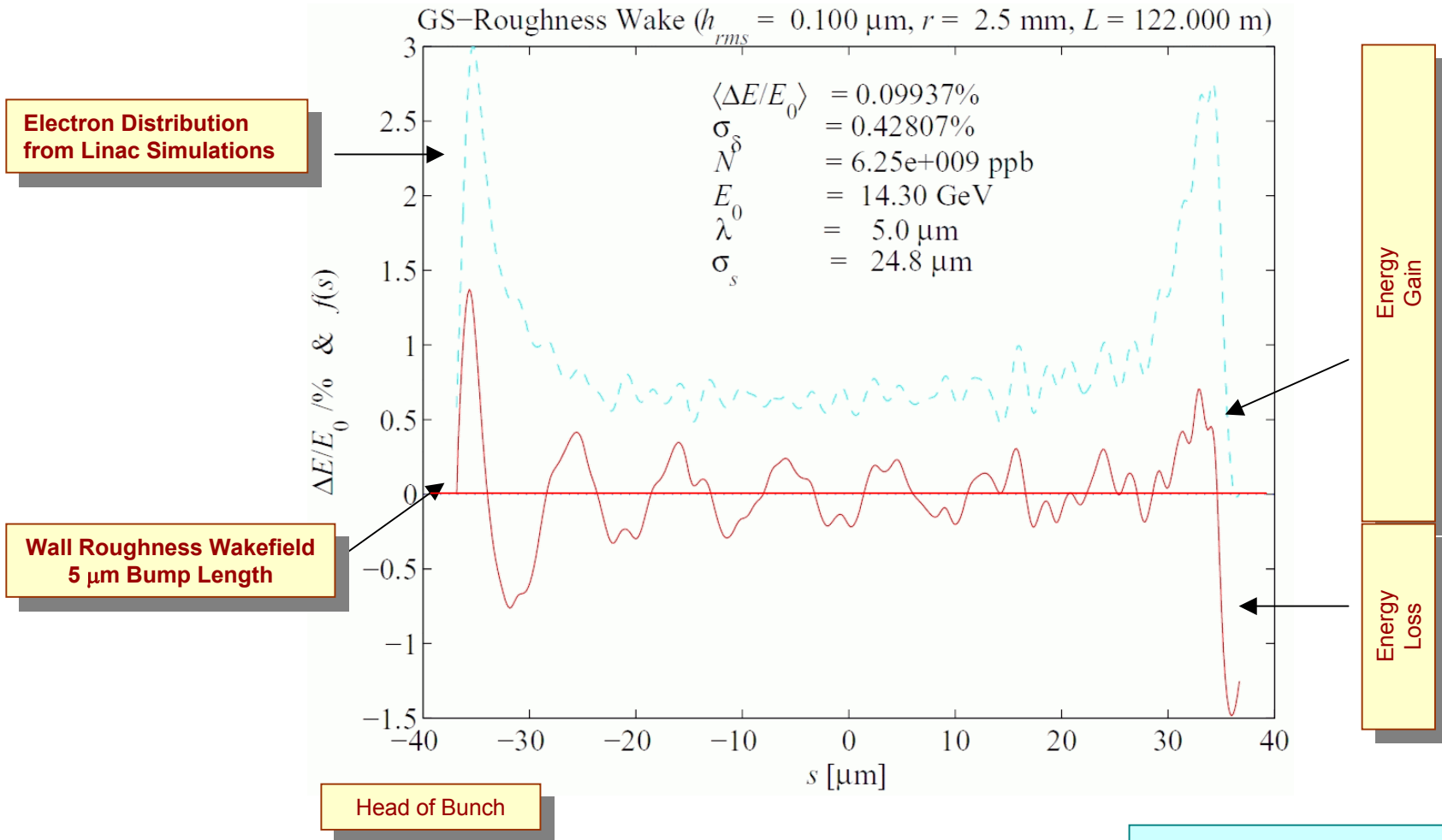
$$W_z(s) = -\frac{cZ_0 e^2}{\pi a^2} \cos(k_0 s)$$

Negligible for aspect ratios > 1 / 1 !

$W_z(s)$	Single Particle Wakefield
Z_0	Vacuum Impedance
a	Pipe Radius
h_0	Corrugation Amplitude
s	Longitudinal Distance from Test Particle to Generator
$p = 2\pi / \kappa$	Corrugation Period
$k_0 = \sqrt{2 p / \delta a g}$	

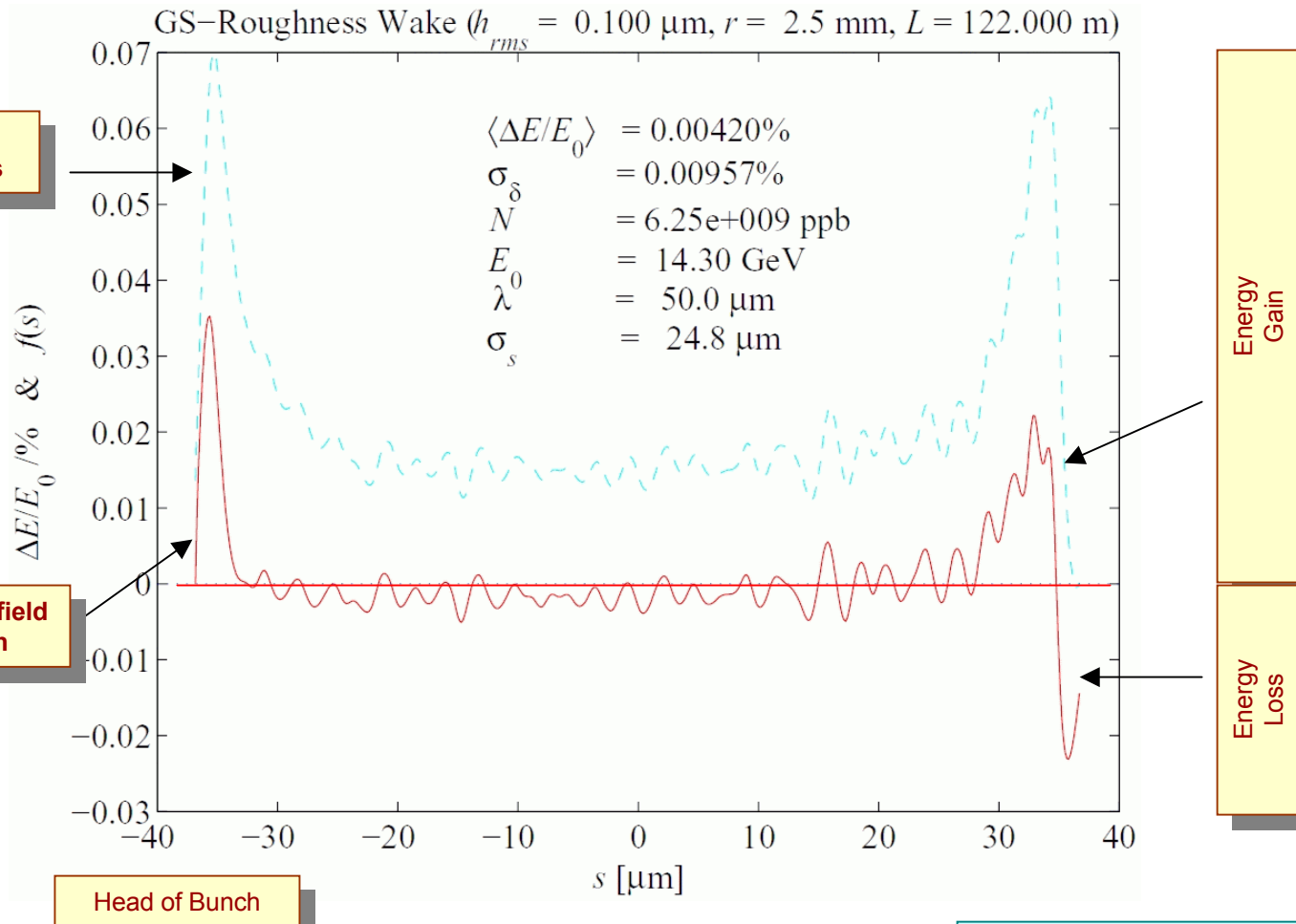


Wall Roughness Wakefield (5 μm / 0.1 μm Bumps) for Simulated Distribution



Courtesy of P. Emma, SLAC

Wall Roughness Wakefield (50 μm / 0.1 μm Bumps) for Simulated Distribution



Courtesy of P. Emma, SLAC

Resistive Wall Wakefield for Short Bunches

Ultra-Relativistic Approximation

$$E_z(s) = -\frac{4ceZ_0}{\pi a^2} \left(\frac{1}{3} e^{-s/s_0} \cos(\sqrt{3}s/s_0) - \frac{\sqrt{2}}{\pi} \int_0^\infty \frac{x^2}{x^6 + 8} e^{-sx^2/s_0} dx \right) \quad z > 0$$

$$E_z(s) = 0 \quad z < 0$$

$$s_0 = \sqrt[3]{\frac{2a^2}{Z_0\sigma}} = 8.3 \mu\text{m}$$

for LCLS Parameters, i.e.,

$a = 2.5 \text{ mm}$

Copper Plated Vacuum Chamber

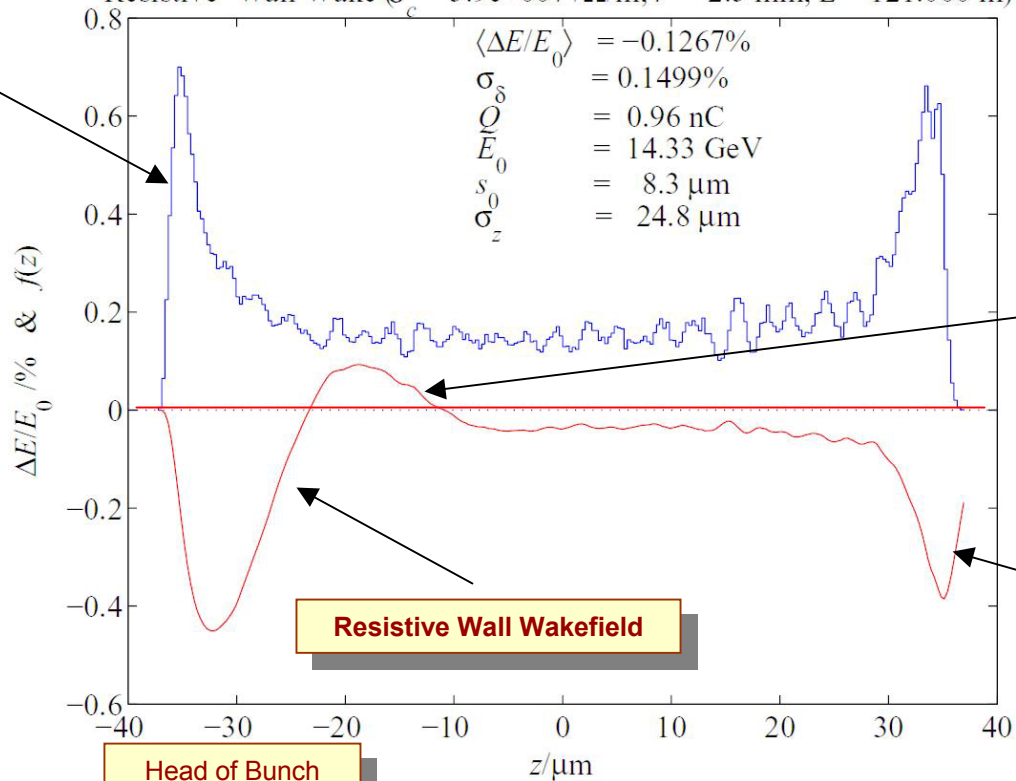
$E_z(s)$	Wakefield Green's Function [V/C/m]
Z_0	Vacuum Impedance
a	Pipe Radius
σ	Conductivity of Vacuum Chamber Material ($5.9 \times 10^7 \Omega^{-1}\text{m}^{-1}$ for Copper)
s	Longitudinal Distance from Test Particle to Generator

Resistive Wall Wakefield for Simulated Distribution

Resistive-Wall Wake ($\sigma_c = 5.9e+007 / \Omega/m, r = 2.5 \text{ mm}, L = 121.000 \text{ m}$)

Electron Distribution
from Linac Simulations

285 keV/m corresponds to 0.2 %
Slice Energy Change per 100 m.



Courtesy of P. Emma, SLAC

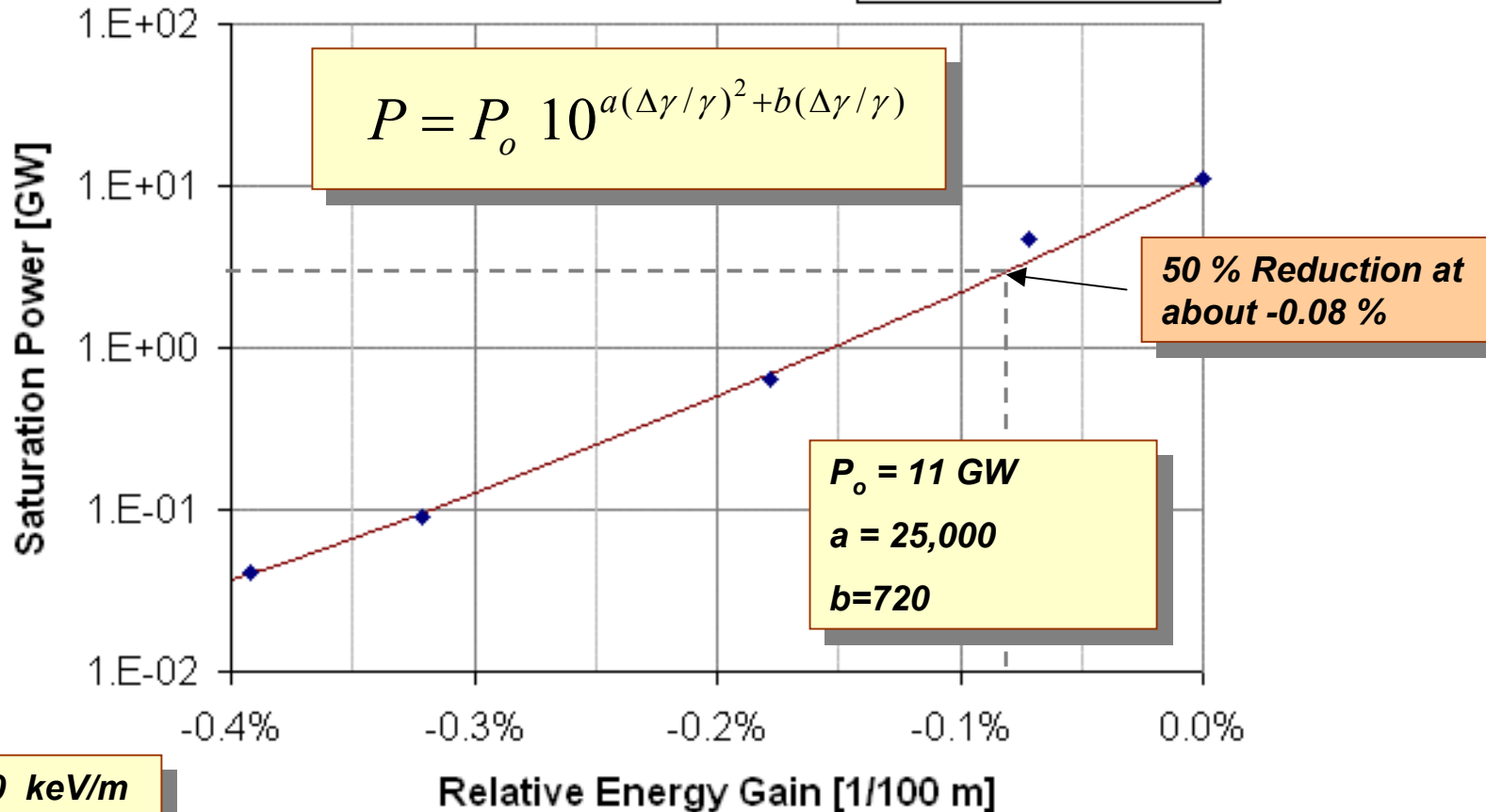
Undulator Wakefield Simulations

Continuous Change in Average Slice Energy along Undulator

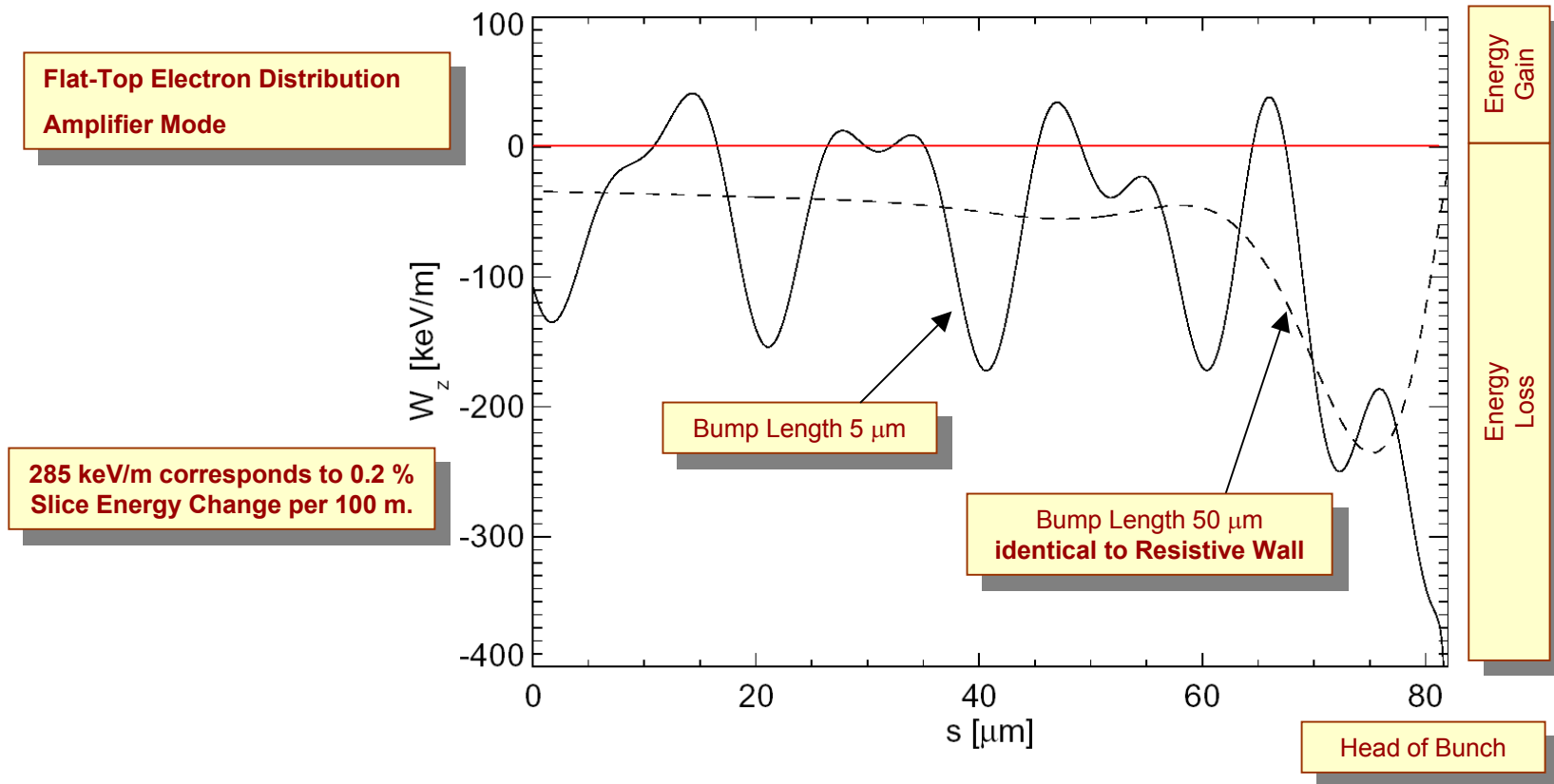
Undulator Wakefield Effects on FEL Performance

1.5 Å

GINGER Simulations



Wakefields used in FEL Simulations



- **Resistive Wall: Copper Plated Stainless Steel**
- **Surface Roughness: Both inductive model and synchronous mode, assuming a 1 nC electron bunch, a bump height of 100 nm**

Courtesy of S. Reiche, UCLA

Undulator Wakefield Simulations : Power Envelope

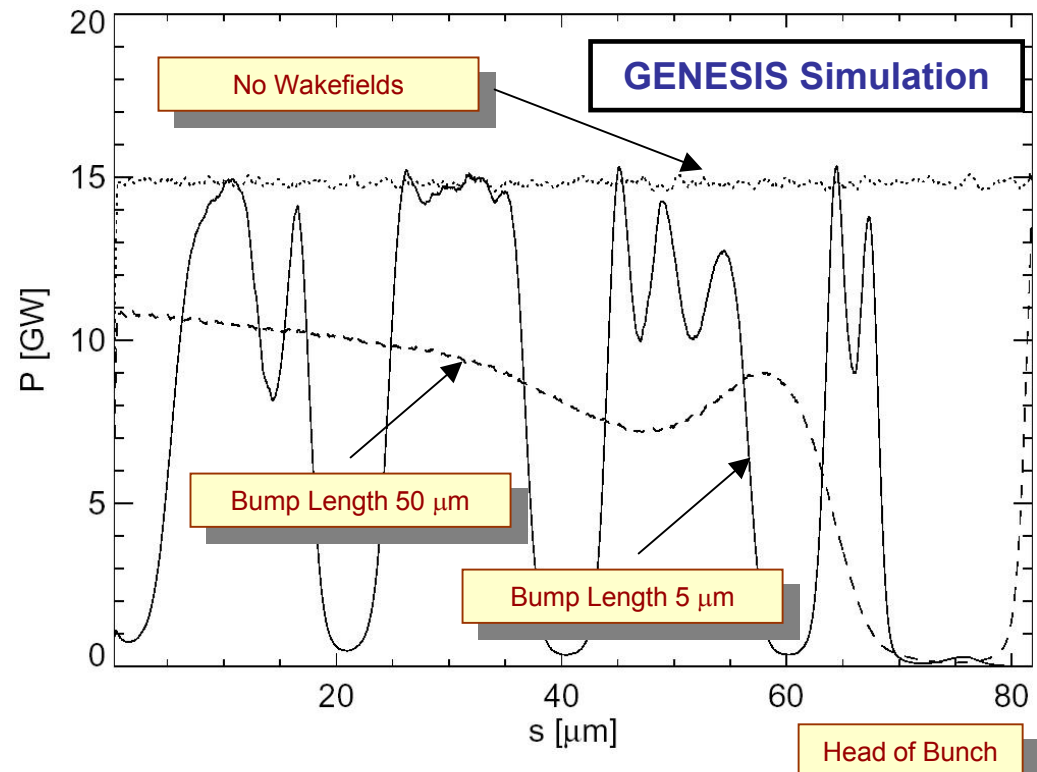
Flat-Top Electron Distribution
Amplifier Mode

Effect of Wakefields on
temporal Radiation Power Profile at
Undulator Exit

Dotted line: no wakefields;

Dashed line: long bump case;

Solid line: short bump case.



Wakefield Effects on LCLS Performance

Flat-Top Electron Distribution
Amplifier Mode

$\epsilon_n = 1.2 \mu\text{m rad}$
 $I_{pk} = 3.4 \text{ kA}$

No Wakefields

Power vs. undulator length
for the LCLS case

Saturation length ~ 92 m

Saturation power levels:

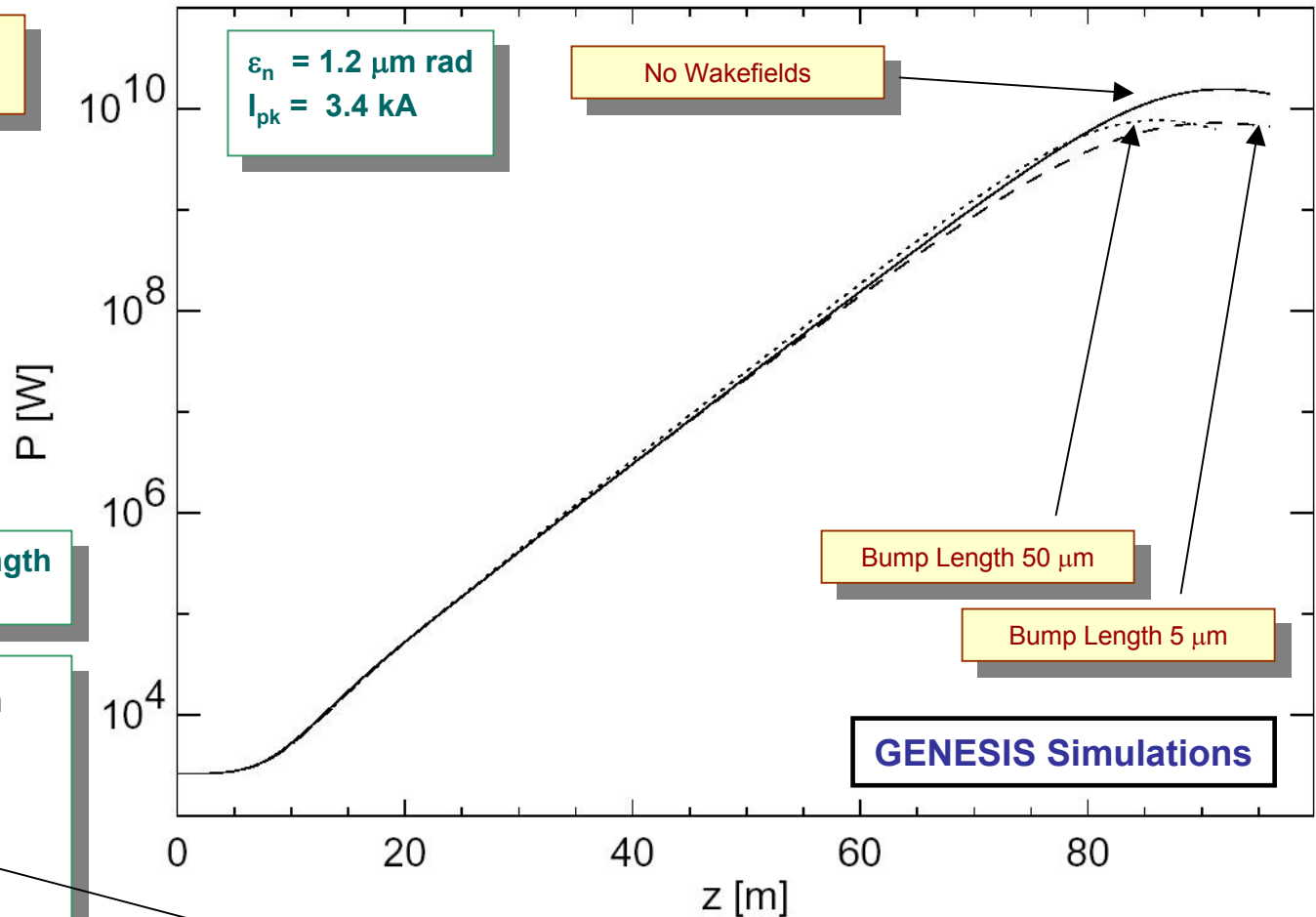
- 15 GW
- 8 GW
- 8 GW
- 7 GW

LCLS Goal Power Level

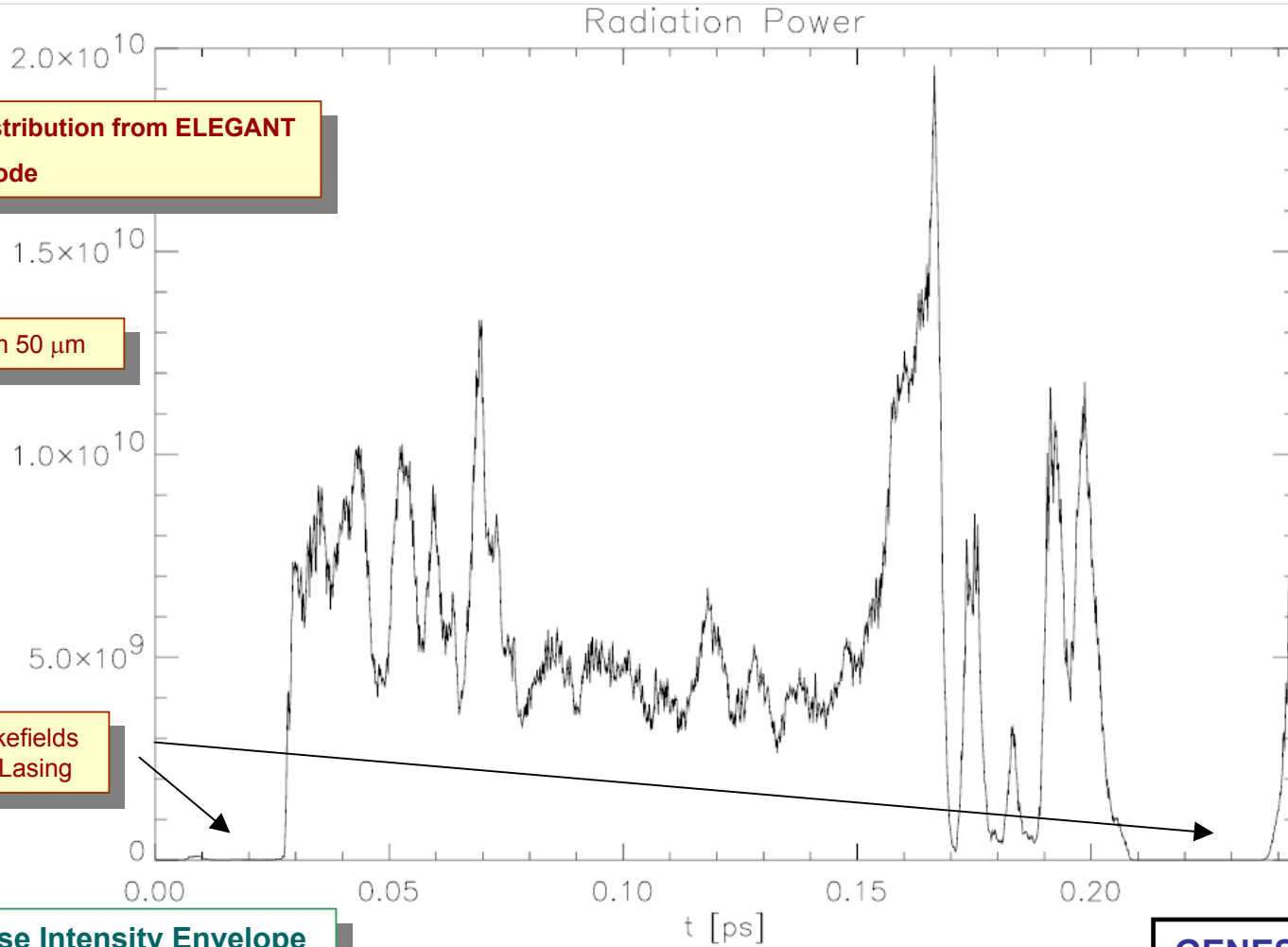
Bump Length 50 μm

Bump Length 5 μm

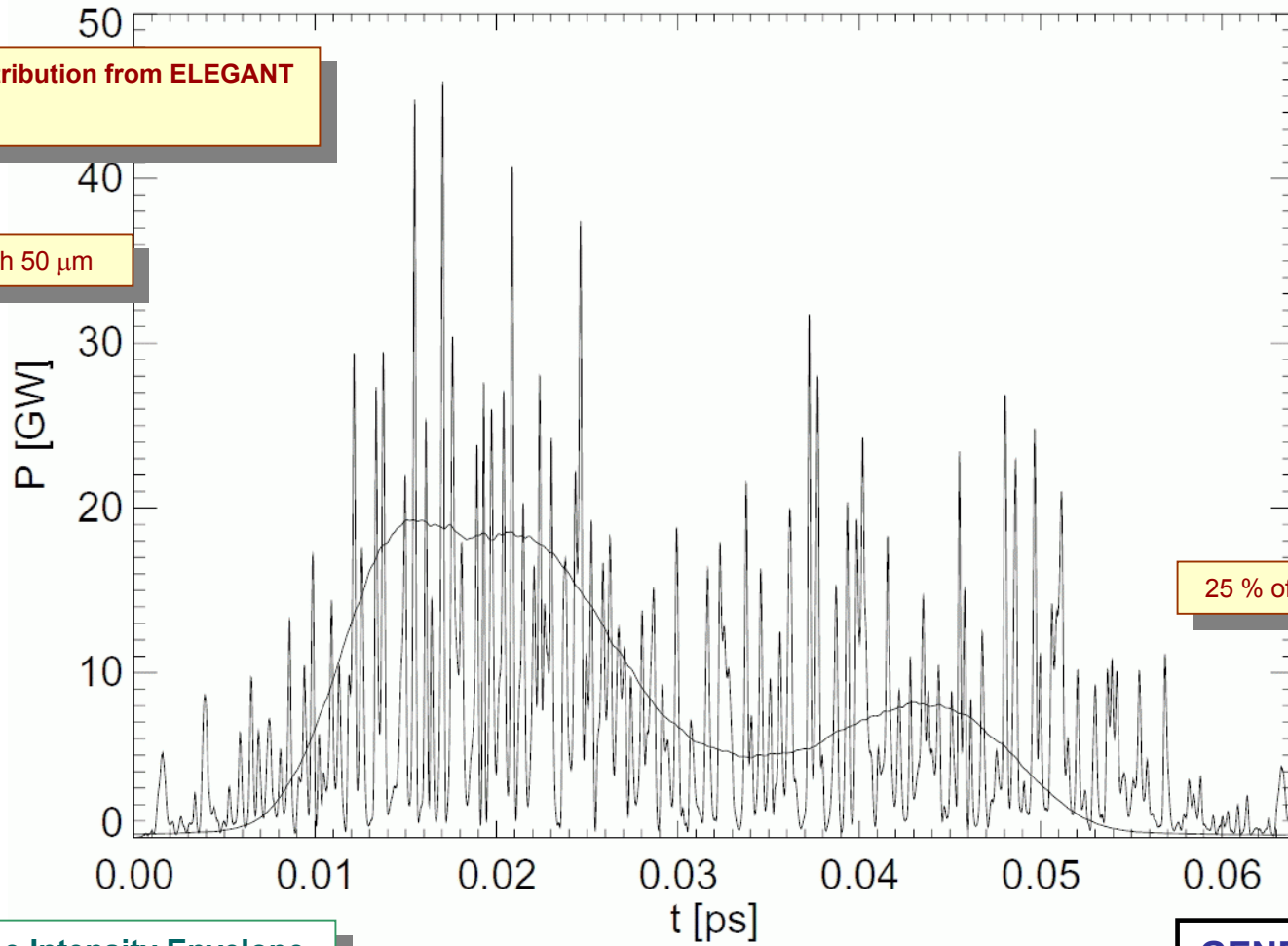
GENESIS Simulations



Wakefield Effects on LCLS Performance A



Wakefield Effects in SASE Simulations



Wakefield Effects on Electron Beam Slices

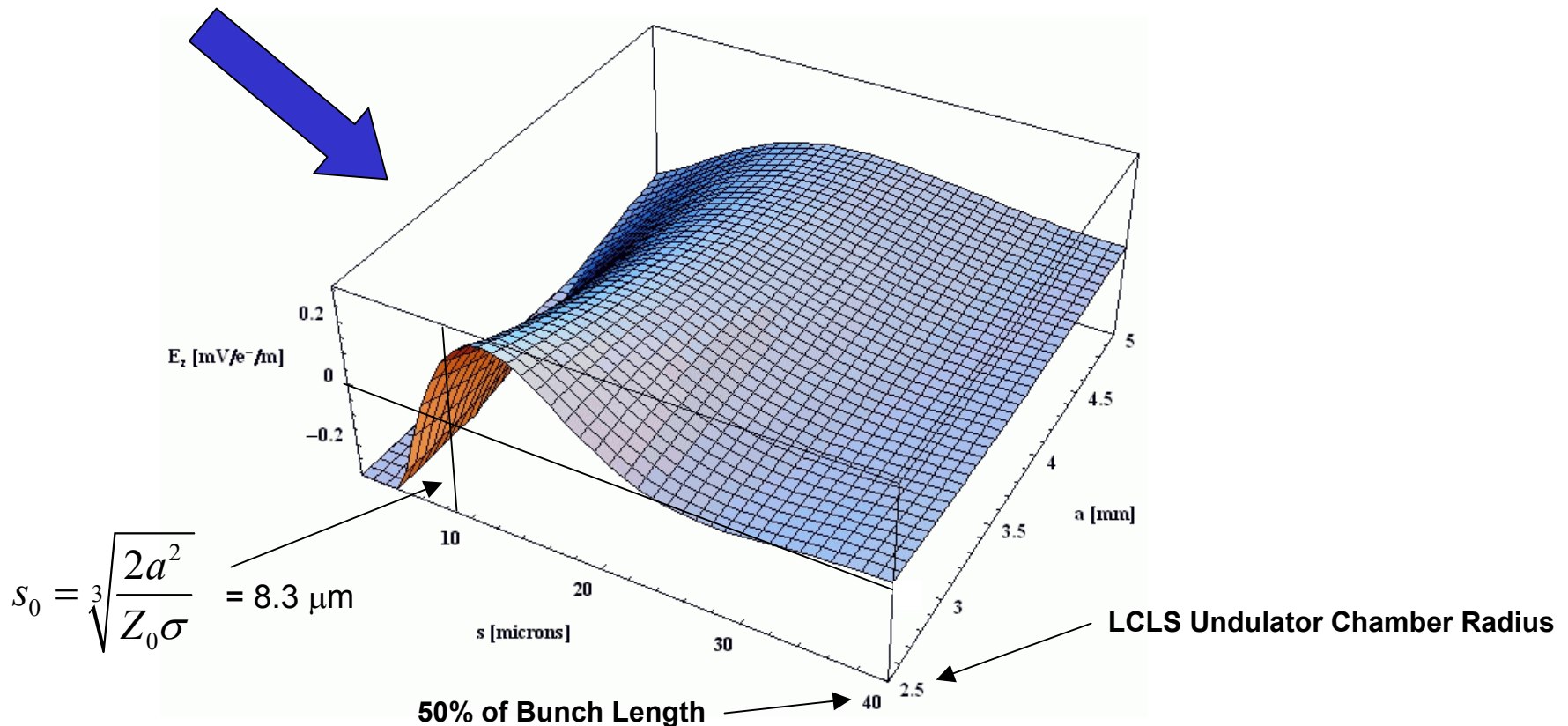
- ***Reduction of Total Pulse Power by about 50%***
7-8 GW instead of 15 GW
- ***Added Temporal Structure in x-ray intensity (Shorter Pulses)***
- ***Practically no Change in Saturation Length***
- ***Radiation Bandwidth increase small (< 30% for unchirped beam)***
- ***Small Decrease in Brightness***

PRESENT LCLS POSITION

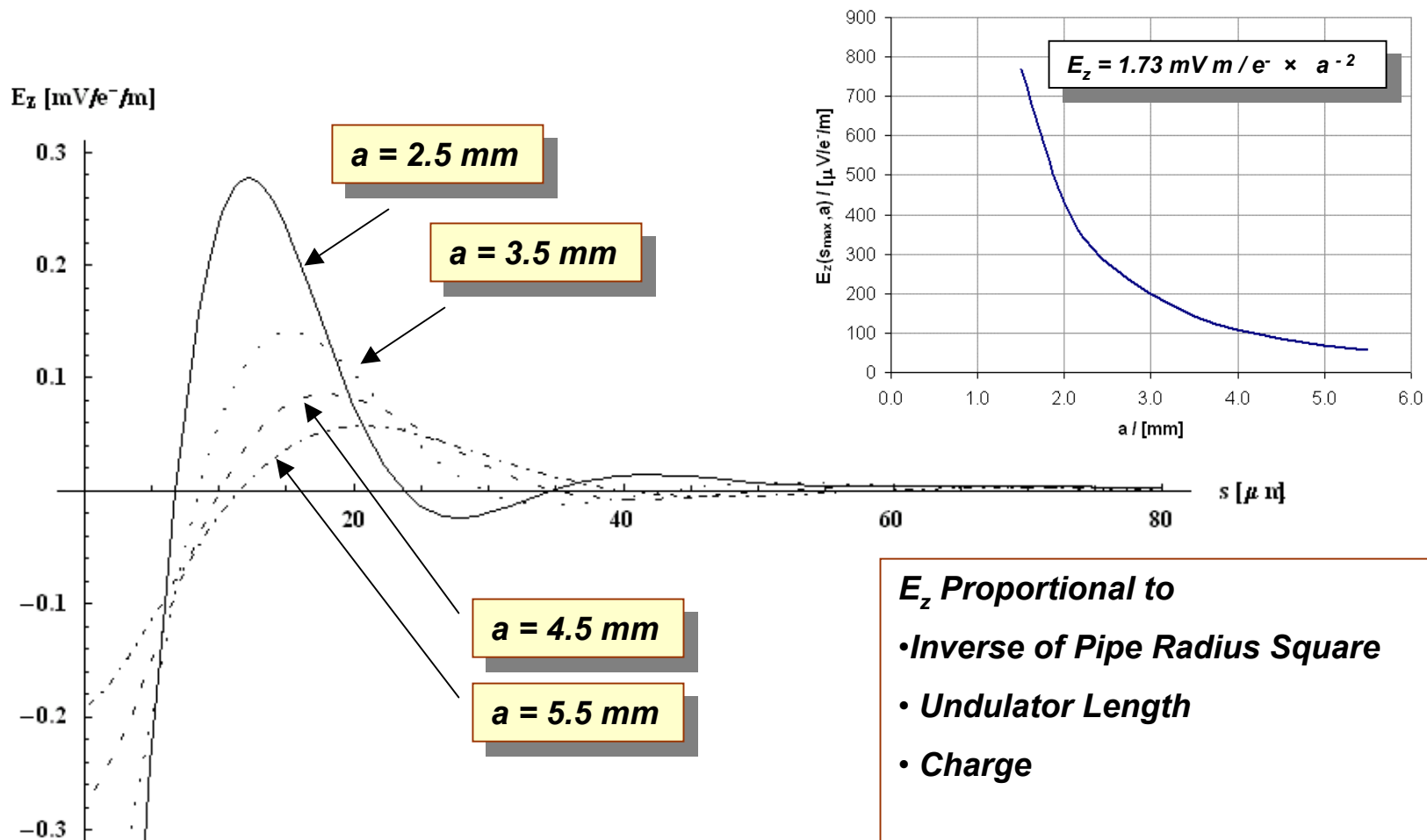
Wakefield Effects do not degrade performance below the design goal.

Resistive Wall Wakefield Sensitivity to Pipe Radius

$$E_z(s, a) = -\frac{4ceZ_0}{\pi a^2} \left(\frac{1}{3} e^{-s/s_0(a)} \cos(\sqrt{3}s / s_0(a)) - \frac{\sqrt{2}}{\pi} \int_0^\infty \frac{x^2}{x^6 + 8} e^{-sx^2/s_0(a)} dx \right)$$



Resistive Wall Wakefield Scaling



E_z Proportional to

- Inverse of Pipe Radius Square
- Undulator Length
- Charge

$$\frac{1}{a^2}$$

$$L_u$$

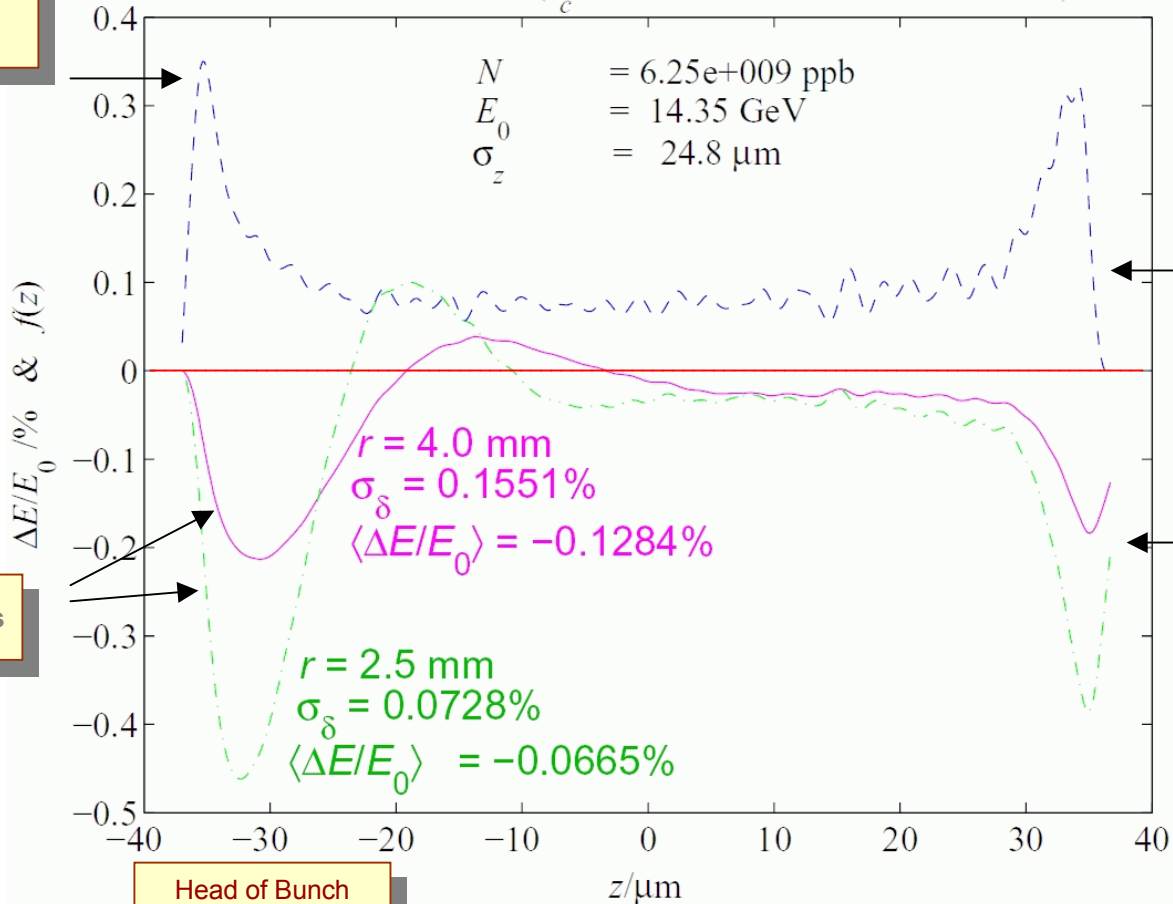
$$Q$$

Resistive Wall Wakefield at 2.5 and 4 mm Radius for Simulated Distribution

Electron Distribution from Linac Simulations

Resistive-Wall Wake ($\sigma_c = 5.9e+007 / \Omega/m, L = 121.000 \text{ m}$)

$N = 6.25e+009 \text{ ppb}$
 $E_0 = 14.35 \text{ GeV}$
 $\sigma_z = 24.8 \mu\text{m}$



Reduction less than quadratic

Head of Bunch

Energy Gain

Energy Loss

Courtesy of P. Emma, SLAC

Summary

- Considered Various Undulator Chamber Wakefields:
 - Geometric
 - Flange Gaps, Pump Slots, BPMs, Shielded Bellows → Negligible Effect
 - Surface Roughness
 - AFM Measurements indicate large Aspect Ratio → Small Effect
 - Resistive Wall
 - Copper Surface → Sizeable Effect
- Resistive wall wakefields in the undulator vacuum chamber effect FEL output for the parameters that are presently proposed for the CDR.
- Total output power expected to be at the goal values as described in the CDR.

Undulator Chamber Wakefields

Heinz-Dieter Nuhn, SLAC / SSRL - December 10, 2001